

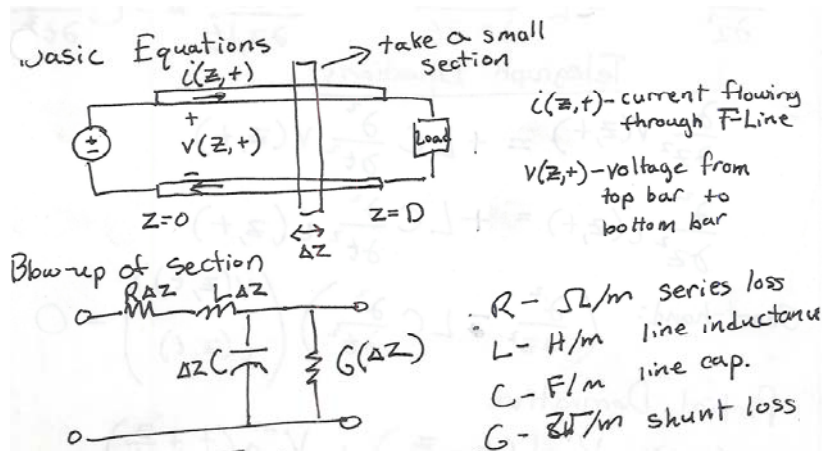
TDT2: Transmission Line Equations

By Prof. Gregory D. Durgin



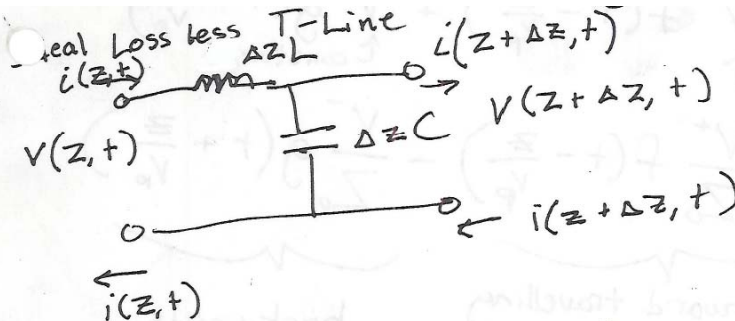
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Circuit Model for a Transmission Line



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Segment Circuit Model



$$-V(z + \Delta z, t) + V(z, t) = \Delta z L \frac{\partial i(z, t)}{\partial t}$$

$$-i(z + \Delta z, t) + i(z, t) = \Delta z C \frac{\partial V(z, t)}{\partial t}$$

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The Telegrapher's Equations

Limit $\Delta z \rightarrow 0$

$$\frac{\partial V(z, t)}{\partial z} = -L \frac{\partial i(z, t)}{\partial t} \quad \frac{\partial i(z, t)}{\partial z} = -C \frac{\partial V(z, t)}{\partial t}$$

$$\frac{\partial^2 V(z, t)}{\partial z^2} = -L \frac{\partial^2 i(z, t)}{\partial z \partial t} \quad \frac{\partial^2 i(z, t)}{\partial z \partial t} = -C \frac{\partial^2 V(z, t)}{\partial t^2}$$

Telegraph Equations

$$\frac{\partial^2 V(z, t)}{\partial z^2} = +LC \frac{\partial^2 V(z, t)}{\partial t^2}$$

$$\frac{\partial^2 i(z, t)}{\partial z^2} = +LC \frac{\partial^2 i(z, t)}{\partial t^2}$$

Short-hand: $\begin{pmatrix} \frac{\partial^2}{\partial z^2} - LC \frac{\partial^2}{\partial t^2} \end{pmatrix} \begin{pmatrix} V(z, t) \\ i(z, t) \end{pmatrix} = 0$

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Solution to the Telegrapher's Equations

Partial Derivative

$$V(z,t) = V^+ f\left(t - \frac{z}{v_p}\right) + V^- g\left(t + \frac{z}{v_p}\right)$$

constant \uparrow constant

$$i(z,t) = \frac{V^+}{Z_0} f\left(t - \frac{z}{v_p}\right) - \frac{V^-}{Z_0} g\left(t + \frac{z}{v_p}\right)$$

$$Z_0 = \sqrt{\frac{L}{C}}$$

$$v_p = \frac{1}{\sqrt{LC}}$$

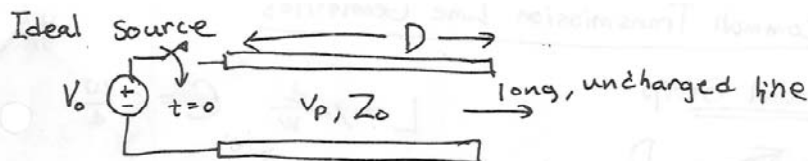
forward travelling wave

backwards travelling wave

The shape of the functions f and g are determined by boundary conditions on the line. (Sources and loads connected to the line.)

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excitation: $V_0 u(t) = f(t)$

boundary condition excitation = $V(0, t)$ on line

$$V(z,t) = V_0 u\left(t - \frac{z}{v_p}\right)$$

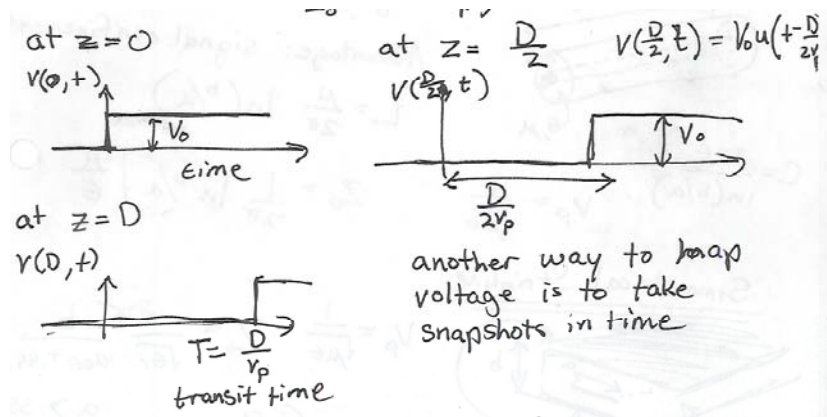
$$i(z,t) = \frac{V_0}{Z_0} u\left(t - \frac{z}{v_p}\right)$$

at $z=0$

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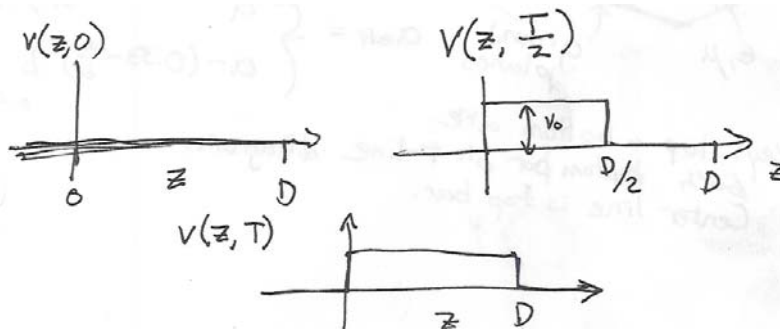
Movement of a Pulse Over Time



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Movement of a Pulse Over Space



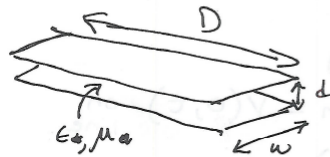
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Parallel Strip Transmission Lines

Common Transmission Line Geometries

Parallel Strip



$$L = \mu \frac{d}{w} \quad C = \epsilon \frac{w}{d}$$

$$V_p = \frac{1}{\sqrt{\mu \epsilon}}$$

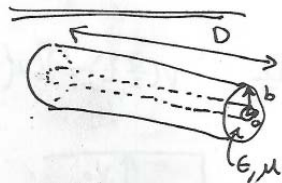
$$Z_0 = \frac{d}{w} \sqrt{\frac{\mu}{\epsilon}}$$

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Coaxial Cable

Coaxial Cable



a - inner radius
b - outer radius

Advantage: signal confinement

$$L = \frac{\mu}{2\pi} \ln(b/a)$$

$$C = \frac{2\pi\epsilon}{\ln(b/a)}$$

$$V_p = \frac{1}{\sqrt{\mu \epsilon}}$$

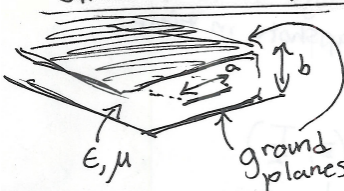
$$Z_0 = \frac{1}{2\pi} \ln b/a \sqrt{\frac{\mu}{\epsilon}}$$

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Symmetrical Stripline

Symmetrical Stripline



$V_p = \frac{1}{\sqrt{\mu\epsilon}}$ $Z_0 = \frac{30\pi}{\sqrt{\epsilon_r}} \frac{b}{a_{eff} + 1.41b}$

$$a_{eff} = \begin{cases} a & a > 3.5b \\ a - (0.33 - \frac{a}{b})^2 b & a < 0.35b \end{cases}$$

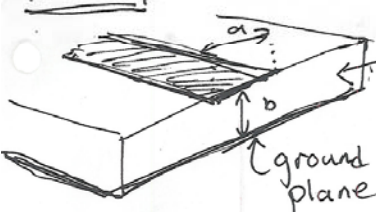
Key: top + bottom are both bottom bar on t-line diagram.
Center line is top bar.

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Microstrip Line

Microstrip 5/5



$\epsilon_{eff} = \epsilon_0 \left[\frac{\epsilon_r + 1}{2} + \frac{\epsilon_r - 1}{2} \frac{1}{\sqrt{1 + 12b/a}} \right]$

$V_p = \frac{1}{\sqrt{\mu\epsilon_{eff}}}$

$$Z_0 = \begin{cases} \frac{1}{2\pi} \sqrt{\frac{\mu}{\epsilon_{eff}}} \ln \left(\frac{8b}{a} + \frac{a}{4b} \right) & a < b \\ \sqrt{\frac{\mu}{\epsilon_{eff}}} \frac{1}{\frac{a}{b} + 1.393 + 0.667 \ln \left(\frac{a}{b} + 1.444 \right)} & a > b \end{cases}$$

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Example Calculation

Example A coaxial cable with inner radius 1mm, outer radius 12mm, and dielectric $\epsilon_r = 24$.

$b = 0.012$
 $a = 0.001$

$L = \frac{\mu_0}{2\pi} \ln\left(\frac{0.012}{0.001}\right) = 5.0 \times 10^{-7} \text{ H/m}$
 always assume μ_0 if not told otherwise

$C = \frac{2\pi\epsilon_r\epsilon_0}{\ln\left(\frac{0.012}{0.001}\right)} = 5.4 \times 10^{-11} \text{ F/m}$

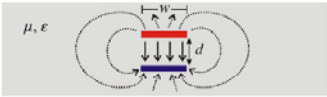
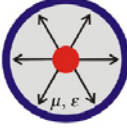
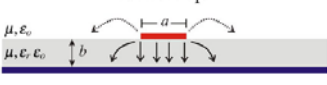
$v_p = \frac{1}{\sqrt{LC}} = 1.9 \times 10^8 \text{ m/s}$

$Z_0 = \sqrt{\frac{L}{C}} = 96 \Omega$

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Summary of Transmission Line Topologies

<p>Parallel Plate</p> 	$L = \mu \frac{d}{w}$ $C = \epsilon \frac{w}{d}$ $v_p = \frac{1}{\sqrt{\mu\epsilon}}$ $Z_0 = \frac{d}{w} \sqrt{\mu/\epsilon}$
<p>Coaxial Cable</p>  <p>inner conductor radius, a outer conductor radius, b</p>	$L = \frac{\mu}{2\pi} \ln(b/a)$ $C = \frac{2\pi\epsilon}{\ln(b/a)}$ $v_p = \frac{1}{\sqrt{\mu\epsilon}}$ $Z_0 = \frac{\ln(b/a)}{2\pi} \sqrt{\mu/\epsilon}$
<p>Microstrip</p> 	$Z_0 = \begin{cases} \frac{1}{2\pi} \sqrt{\mu/\epsilon_{eff}} \ln\left(\frac{8b}{a} + \frac{a}{4b}\right), & a < b \\ \frac{1}{\sqrt{\mu/\epsilon_{eff}}} \frac{1}{ab + 1.393 + 0.667 \ln(ab + 1.444)}, & a > b \end{cases}$ $\epsilon_{eff} = 8.854 \times 10^{-12} \left[\frac{\epsilon_r + 1}{2} + \frac{\epsilon_r - 1}{2} \frac{1}{\sqrt{1 + 12b/a}} \right] \text{ F/m}$ $v_p = \frac{1}{\sqrt{\mu\epsilon_{eff}}}$ $L = \frac{Z_0}{v_p}$ $C = \frac{1}{Z_0 v_p}$

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Other Transmission Line Topologies

<p>Stripline</p>	$a_{eff} = \begin{cases} a, & a > 0.35b \\ a - \left(0.35 - \frac{a}{b}\right)^2 b, & a < 0.35b \end{cases}$ $L = \frac{Z_0}{v_p}$ $Z_0 = \frac{30\pi}{\sqrt{\epsilon_r}} \frac{b}{a_{eff} + 0.441b} \quad v_p = \frac{1}{\sqrt{\mu\epsilon_r}} \quad C = \frac{1}{Z_0 v_p}$
<p>Two Wires / Twin Lead</p>	$L = \frac{\mu}{\pi} \cosh^{-1} \left(\frac{b}{2a} \right) \quad C = \frac{\pi\epsilon}{\cosh^{-1} \left(\frac{b}{2a} \right)}$ $Z_0 = \frac{1}{\pi} \sqrt{\frac{\mu}{\epsilon}} \cosh^{-1} \left(\frac{b}{2a} \right) \quad v_p = \frac{1}{\sqrt{\mu\epsilon}}$
<p>Coplanar Strip</p>	$Z_0 = \sqrt{\frac{\mu}{\epsilon_{eff}}} \frac{K(a/b)}{K(\sqrt{1-a^2/b^2})} \quad \epsilon_{eff} = 8.854 \times 10^{-12} \left(\frac{\epsilon_r + 1}{2} \right) \text{ F/m}$ $K(k) = \int_0^{\pi/2} \frac{d\phi}{\sqrt{1-k^2 \sin^2 \phi}} \quad \text{complete elliptic integral, 1st kind} \quad v_p = \frac{1}{\sqrt{\mu\epsilon_{eff}}}$

Key: + Conductor \longrightarrow Confined Electric Field $\mu = (4\pi \times 10^{-7}) \mu_r$ (H/m)
 Dielectric $\cdots\cdots\longrightarrow$ Fringing Electric Field $\epsilon = (8.854 \times 10^{-12}) \epsilon_r$ (F/m)

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