

In this module, we look to treat and analyze an antenna in the context of circuit theory. One of the key outcomes of our discussion is to understand how to model antennas with circuit theories, as well as how to translate between the world of voltage and power at the terminals of an antenna.



If we are transmitting with an antenna, it will look like a complex load Z\_A at the end of the transmission line with intrinsic impedance Z\_0. The source, say an RF power amplifier, sends a signal to the impedance-modeled antenna through a transmission line. If it is a good antenna, most of the power absorbed by this load represents radiated power.



How much power is delivered to an antenna with a source of amplitude  $V_s$ ? Here is a basic analysis of the total power delivered to the load. This expression above is for time-averaged, real power based on a phasor representation of voltage and current.



The above expression illustrates how much power is absorbed by a load impedance.

Of course, maximum power transfer occurs when the load is conjugate-matched with the source impedance. Thus, when the imaginary portion of the load impedance is opposite valued from the imaginary value of the source impedance and the real value of the impedances are identical, the maximum amount of power is transferred to the load. The expression for this is shown above.



This illustrates one of the classical engineering problems in antenna engineering: matching an antenna to a lossless transmission line (real impedance). Usually, antennas are designed for pattern, gain, polarization, and a variety of other radiation characteristics. The resulting impedance is a secondary concern; thus, the impedance off the design table is rarely matched to the actual feed line without additional engineering work.

One key task of the antenna engineer is to design a matching network to transmission line/source. The matching network is usually a low-loss portion of circuitry consisting of either discrete capacitors and inductors or stubs and other resonant t-line structures that provides a Z\_0-equivalent impedance at the end of a transmission line ... all with the intention of providing maximum power transfer to the antenna. This is important, since any reflected power in such a system represents a waste that burns unnecessary power or reduces signal integrity at a receiver.



We may also view the antenna in a circuit when it is used to receive a signal. In this case, by virtue of the reciprocity theorem in electromagnetics, the antenna has the same intrinsic impedance whether it functions as a transmitter or a receiver. The power that an antenna delivers to a complex load is shown above.



Here, the maximum power delivered to the conjugate-matched load is shown in the top formula. From this, we can back-solve the voltage of the terminals of a matched antenna if given the power. This is particularly useful, since the received power of a link budget usually assumes matched antennas. What if a different load is attached to the matched antenna? If so, the amplitude of the voltage at that terminal will change. The bottom equation shows how to compute this amplitude given the impedance of the load and antenna as well as the ideal "link budget" received power.



**Example 1: Amplitude on a Charge Pump** Example A 50-De antenna receives 10 dBm of power and is connected to a microwave energy-harvesting circuit with impedance 30-j100se. What must the threshold voltage be (may) of the energy-harvesting diodes in this circuit? Georgia Emag copyright 2009 – all rights reserved

Solution 1: Amplitude on a Charge Pump
Ans $R_A = 50 \Omega  X_A = 0$ $R_L = 30 \Omega  X_2 = -100 \Omega  (3)$ $S = 50 \Omega  X_2 = -100 \Omega  (3)$
$V_{A} = \frac{2 \left[ 30^{2} + 100^{2} \right]^{\frac{1}{2} \cdot 50 \cdot 0.01}}{\left[ (50 + 30)^{2} + (0 + 100)^{2} \right]^{\frac{1}{2}}}$
$= 2 \tilde{z}_{L} JZRRR = 0.16 V$ $ \tilde{z}_{L} + \tilde{z}_{A} $ What would make this higher?
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