

# ANT1: Basic Radiation Theory

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# Radiation from Impressed Currents

Helmholtz presumes free-space, source-free medium. But if we want to study radiation patterns from current distributions, we need sources.

$$\begin{array}{c} \nearrow \\ \uparrow \\ \nearrow \end{array} \tilde{\mathbf{J}}(\vec{r})$$

$$\begin{aligned} \nabla \times \tilde{\mathbf{H}} &= j\omega\epsilon \tilde{\mathbf{E}} + \tilde{\mathbf{J}} \quad \leftarrow \begin{array}{l} \text{impressed} \\ \text{current} \end{array} \\ \nabla \times \tilde{\mathbf{E}} &= -j\omega\mu \tilde{\mathbf{H}} \end{aligned}$$

Two types of Antenna problems

- Know the currents a priori, solve for radiation
- need to solve for radiation and current distribution (chicken and egg problem).

# Introduction of Vector Magnetic Potential

## Radiation from Impressed Currents

Electric Potential

$$\vec{E} = -\nabla\phi_e$$

(vector)  
Magnetic Potential

$$\vec{H} = \frac{1}{\mu} \nabla \times \vec{A}$$

Thus

$$\nabla \times \vec{E} = -j\omega\mu\vec{H} = -j\omega\nabla \times \vec{A}$$

implies

$$\vec{E} = -j\omega\vec{A} - \nabla\phi_e$$

← this one always curls to zero

# Development of a Scalar Wave Equation

Now

$$\nabla \times \tilde{\mathbf{H}} = \frac{1}{\mu} \nabla \times \nabla \times \tilde{\mathbf{A}} = j\omega \epsilon \tilde{\mathbf{E}} + \tilde{\mathbf{J}}$$

$$\nabla \times \nabla \times \tilde{\mathbf{A}} = j\omega \epsilon \mu [-j\omega \tilde{\mathbf{A}} - \nabla \tilde{\Phi}_e] + \mu \tilde{\mathbf{J}}$$

$$\nabla(\nabla \cdot \tilde{\mathbf{A}}) - \nabla^2 \tilde{\mathbf{A}} = \underbrace{+\omega^2 \epsilon \mu}_{k^2} \tilde{\mathbf{A}} - j\omega \epsilon \mu \nabla \tilde{\Phi}_e + \mu \tilde{\mathbf{J}}$$

$$(\nabla^2 + k^2) \tilde{\mathbf{A}} - \nabla(\nabla \cdot \tilde{\mathbf{A}} + j\omega \epsilon \mu \tilde{\Phi}_e) = -\mu \tilde{\mathbf{J}}$$

still have freedom to choose/  
specify  $\nabla \cdot \tilde{\mathbf{A}} = -j\omega \epsilon \mu \tilde{\Phi}_e$

# Scalar Wave Equation

Now

$$(\nabla^2 + k^2)\vec{A} = -\mu\vec{J}$$

Much more solvable. So once we get  $\vec{A}$ ,

$$\vec{H}(\vec{r}) = \frac{1}{\mu} \nabla \times \vec{A} \quad \text{and}$$

$$\vec{E}(\vec{r}) = \frac{1}{j\omega\epsilon} \nabla \times \vec{H} = \frac{1}{j\omega\mu\epsilon} \nabla \times \nabla \times \vec{A}$$

## Green's Theorem for Solving the Scalar Wave Equation

Let's assume  $z$ -oriented currents

$$(\nabla^2 + k^2) \tilde{A}_z \hat{z} = -\frac{1}{\mu} J_z(x, y, z) \hat{z}$$

Homogeneous Solution (origin exclusion)

$$(\nabla^2 + k^2) \tilde{A}_z = 0 \quad \tilde{A}_{z1} = C_1 \frac{\exp(-jkr)}{r}$$

non-physical  
"collapsing power"  $\rightarrow$

$$\tilde{A}_{z2} = C_2 \frac{\exp(+jkr)}{r}$$

## Example: Ideal (Hertzian) Dipole

Green's theorem

$$\tilde{A}_z(x, y, z) = \frac{\mu}{4\pi} \iiint \tilde{J}_z(x', y', z') \frac{\exp(-jkR)}{R} dx' dy' dz'$$

$$R = \sqrt{(x-x')^2 + (y-y')^2 + (z-z')^2}$$

Hertzian Dipole

$$\vec{r} = x\hat{x} + y\hat{y} + z\hat{z}$$

$$\tilde{J}_z(\vec{r}) = I \delta(x) \delta(y) \delta(z) = I \delta(\vec{r}) \quad \begin{array}{l} \text{small current} \\ \text{element on} \\ \text{the origin} \end{array}$$

$$\begin{aligned} \tilde{A}_z(x, y, z) &= \frac{\mu I \delta}{4\pi} \frac{\exp(-jk\sqrt{x^2+y^2+z^2})}{\sqrt{x^2+y^2+z^2}} \\ &= \frac{\mu I \delta}{4\pi} \frac{\exp(-jkr)}{r} \end{aligned}$$

## Solution for the Ideal Dipole

Fields from Hertzian Dipole

$$\vec{H}(\vec{r}) = \frac{1}{\mu} \nabla \times (\vec{A}_z \hat{z}) = j \frac{I dl k \sin \theta}{4\pi r} \left(1 + \frac{1}{jkr}\right) \exp(jkr) \hat{\phi}$$

$$\vec{E}(\vec{r}) = \frac{\nabla \times \nabla \times (\vec{A}_z \hat{z})}{j\omega\mu\epsilon} =$$

$$\exp(-jkr) \left[ \frac{k\eta I \cos \theta dl}{2\pi r^2} \left(1 + \frac{1}{jkr}\right) \hat{r} + \frac{kj\eta I dl \sin \theta}{4\pi r} \left(1 + \frac{1}{jkr} - \frac{1}{(kr)^2}\right) \hat{\theta} \right]$$

Usually interested in far field  $kr \gg 1$  ( $r \gg \lambda$ )

$$\vec{H}(\vec{r}) \cong j \frac{I dl k \sin \theta}{4\pi r} \exp(-jkr) \hat{\phi}$$

$$\vec{E}(\vec{r}) \cong j \eta \frac{I dl k \sin \theta}{4\pi r} \exp(-jkr) \hat{\theta}$$



# Ideal Dipole: Total Radiated Power

Usually interested in Power

$$\vec{S}(r, \theta, \phi) = \frac{1}{2} \Re \{ \vec{E} \times \vec{H}^* \} = \frac{I^2 d^2 k^2 \sin^2 \theta \eta}{2(4\pi r)^2} \hat{r}$$

Poynting Vector

Total Power

$$P_T = \iint_A d\hat{n} \cdot \vec{S} = \iint_0^\pi \int_0^{2\pi} \underbrace{r^2 \sin \theta d\theta d\phi}_{d\hat{n}} \cdot \frac{I^2 d^2 k^2 \sin^2 \theta \eta}{32\pi^2 r^2} \hat{r}$$

$$= \frac{I^2 d^2 \eta (2\pi/\lambda)^2}{16\pi} \int_0^\pi \sin^3 \theta d\theta$$

Look-up

$$\int_0^\pi \sin^3 \theta d\theta = \left[ -\cos \theta + \frac{1}{3} \cos^3 \theta \right]_0^\pi$$

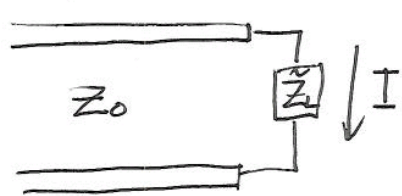
$$= [ -(-1) - \frac{1}{3} ] - [ -1 + \frac{1}{3} ] = \frac{4}{3}$$

Total Power

$$P_T = \frac{I^2 d^2 \eta \pi}{3\lambda^2}$$

# Ideal Dipole: Characteristic Impedance

Characteristic Impedance of Hertzian/  
Ideal Dipole



$$\tilde{Z}_L = R_A + jX_A$$

$\uparrow$  real  $\uparrow$   $\uparrow$  very large for small  $dl$   
 radiation impedance

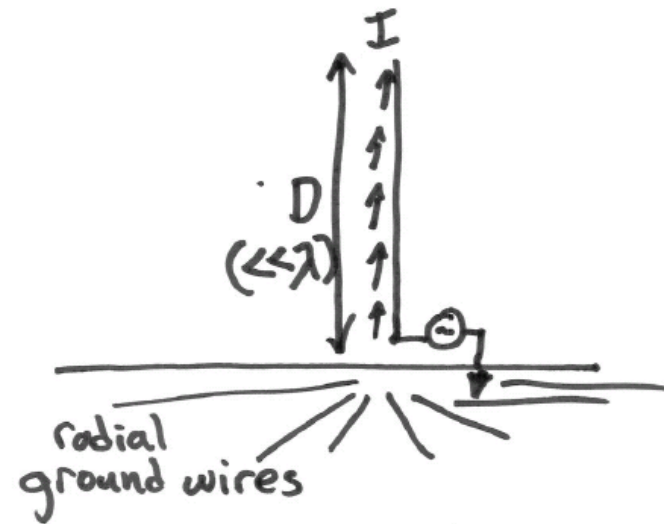
$$P_T = \frac{1}{2} I^2 R_A = \frac{I^2 dl^2 \eta \pi}{3 \lambda^2} \therefore R_A = \frac{2\pi \eta}{3} \left(\frac{dl}{\lambda}\right)^2$$

$$X_A \approx -j Z_0 \cot \frac{2\pi}{\lambda} dl \quad \text{very capacitive}$$

$$\tilde{Z}_L \approx \frac{2\pi \eta}{3} \left(\frac{dl}{\lambda}\right)^2 - j Z_0 \cot \frac{2\pi dl}{\lambda}$$

Mismatch is serious for short antennas

# Examples of Short Dipoles and Mismatch Problems



# Directivity and Gain

$$D(\theta, \phi) = \frac{(4\pi r^2) \|\vec{S}(r, \phi, \theta)\|}{P_T} \leftarrow \text{total radiated power}$$

$$= \frac{(4\pi r^2) \frac{I^2 dl^2 k^2 \sin^2 \theta \eta}{32\pi^2 r^2}}{I^2 dl^2 \eta \pi / 3\lambda^2} = \frac{12\lambda^2 \left(\frac{2\pi}{\lambda}\right)^2 \sin^2 \theta}{32\pi^2}$$

$$= \frac{3}{2} \sin^2 \theta$$

$$\text{Gain} = D(\theta, \phi) \times \eta \leftarrow \begin{array}{l} \text{efficiency} \\ (100\% \text{ for PEC, no} \\ \text{dielectric losses}) \end{array}$$

## Half-Power Beamwidth

$$\text{Max Gain: } 10 \log_{10} \left( D(\theta = \frac{\pi}{2}, \phi) \times 100\% \right) = 1.8 \text{ dB} \\ \text{(3/2 linear)}$$

Half-Power Beamwidth

$$G(\theta'_{\text{HPBW}}, \phi) = \frac{1}{2} G(\theta_{\text{max}} = \frac{\pi}{2}, \phi)$$

$$\frac{3}{2} \sin^2 \theta'_{\text{HPBW}} = \frac{3}{4} \Rightarrow \theta_{\text{HPBW1}} = \frac{\pi}{4}$$

$$\theta_{\text{HPBW2}} = \frac{3\pi}{4}$$

$$\theta_{\text{HPBW}} = \theta_{\text{HPBW2}} - \theta_{\text{HPBW1}} = 90^\circ$$